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DYSCO - A SOFTWARE SYSTEM FOR MODELING GENERAL DYNAMIC SYSTEMS

By

Alex Berman
Kaman Aerospace Corporation
Bloomfield, Connecticut

ABSTRACT

The DYSCO program has been under development since 1979. It has been funded by Army and Air Force laboratories and by the Kaman Aerospace Corporation. It is presently available at a number of government and nongovernment installations. It has been used to analyze a very broad range of dynamics problems.

A principle feature of the software design of DYSCO is the separation of the executive from the technology. The executive, which controls all the operations, is "intelligent" in the sense that it "knows" that its function is to assemble differential equations and to prepare them for solution. The "technology library" contains FORTRAN routines which perform standard functions, such as, computing the equation coefficients of an element (or "component") given the local state at any time. The technology library also contains algorithms and procedures for solving the coupled system equations.

The system was designed to allow easy additional of technology to the library. Any linear or nonlinear structural entity, control system, or set of ordinary differential equations may be simply coded and added to the library, as well as algorithms for time or frequency domain solution.

The program will be described with emphasis on its usefulness in easily modeling unusual concepts and configurations, performing analysis of damage, evaluating new algorithms, and simulating dynamic tests. Illustrations of several typical and illustrative applications will be presented. A summary of the technology presently residing in the technology libraries at the various sites will also be given.

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DYSCO - A SOFTWARE SYSTEM
FOR MODELING GENERAL DYNAMIC SYSTEMS

ALEX BERMAN
KAMAN AEROSPACE CORPORATION

WORKSHOP ON COMPUTATIONAL ASPECTS IN THE CONTROL OF FLEXIBLE SYSTEMS
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INTRODUCTION TO DYSCO

- 0 DYNAMIC SYSTEM COUPLER (DYSCO)
- 0 INITIAL DEVELOPMENT - 1979
- 0 FUNDED BY ARMY, AIR FORCE, KAMAN
- 0 PRESENTLY OPERATIONAL ON IBM AND VAX
- 0 SIZE - 50000+ LINES OF CODE
350+ SUBROUTINES
4+ MEGABYTES OF STORAGE

DEFINITION OF DOMAIN OF DYSCO

DYSCO COUPLES AND SOLVES SECOND ORDER ODE

$$0 \quad M_I \ddot{X}_I + C_I \dot{X}_I + K_I X_I = F_I \quad (\text{COMPONENT } I)$$

$$0 \quad X_I = T_I X_S$$

$$0 \quad M_S \ddot{X}_S + C_S \dot{X}_S + K_S X_S = F_S \quad (\text{SYSTEM})$$

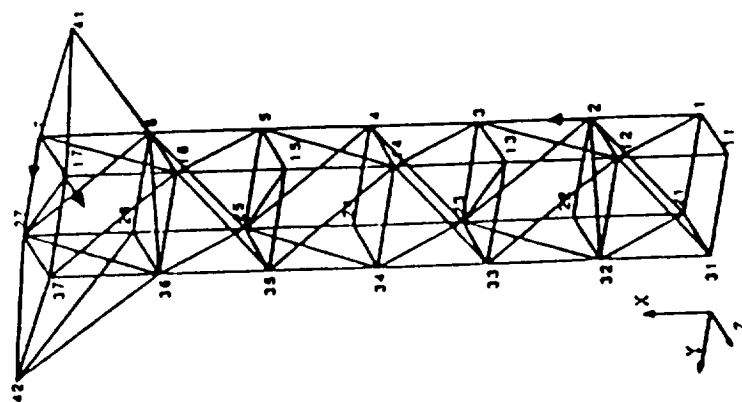
DEFINITION OF COMPONENT

- 0 "COMPONENT" IS MORE GENERAL THAN "FINITE ELEMENT"
- 0 M_I, C_I, K_I, F_I = ARBITRARY FUNCTIONS OF STATE
- 0 X_I = ANY GENERALIZED DOF - PHYSICAL, MODAL, OTHER
- 0 COMPONENT MAY BE
 - FINITE ELEMENT
 - ASSEMBLY OF FINITE ELEMENTS (SUBSYSTEM, OUTPUT OF FE ANALYSIS)
 - SPECIAL SET OF EQUATIONS (E.G., HELICOPTER ROTOR, SPECIAL MECHANISM)
 - CONTROL ALGORITHM (MIMO, NON-SYMMETRICAL MATRICES, NONLINEAR)
 - FORCE ALGORITHM (M, C, K = NULL, AERO, ELECTROMAGNETIC)
 - ETC., ETC.

DEFINITION OF MODEL

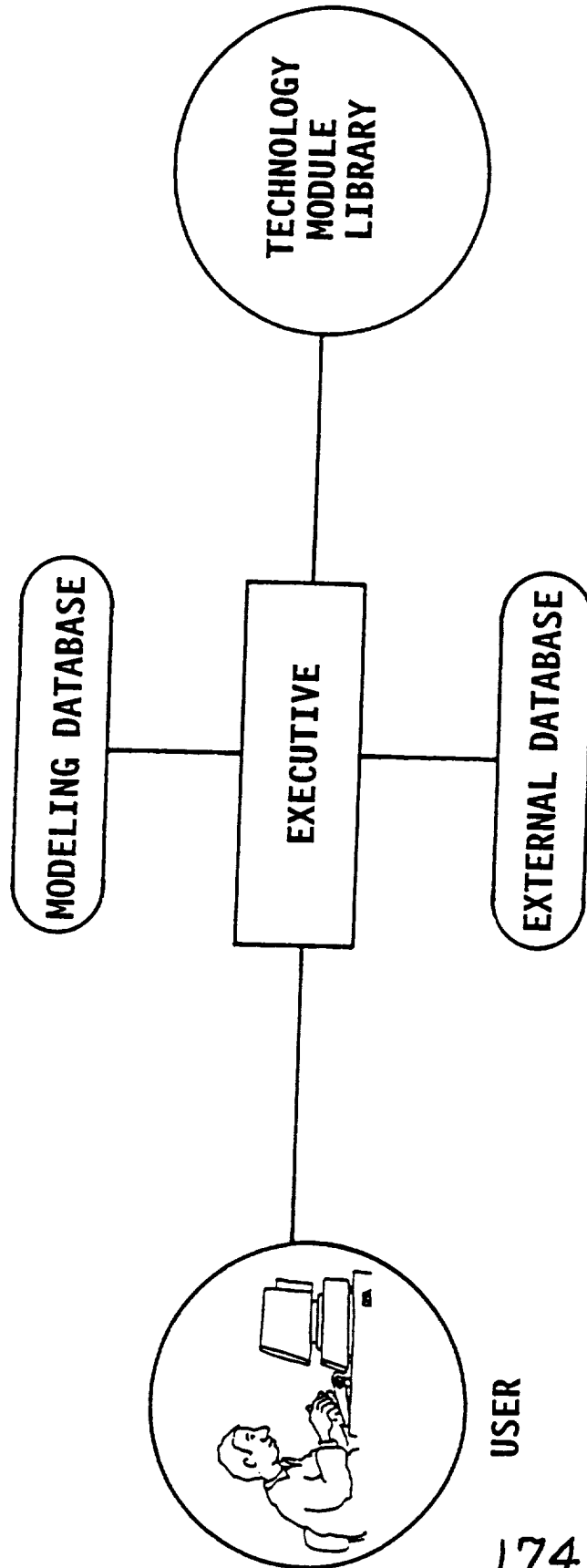
- 0 A MODEL IS A DESCRIPTION OF A COUPLED SET OF COMPONENT EQUATIONS
- 0 COMPONENT EQUATIONS ARE DEFINED BY
 - NAME OF THE ALGORITHM IN "TECHNOLOGY LIBRARY"
 - NAME OF DATA SET IN "MODELING DATABASE"
- 0 COMMAND "RUN" COUPLES EQUATIONS
- 0 NEXT STEP IS TO SPECIFY SOLUTION ALGORITHM

ILLUSTRATIVE MODEL

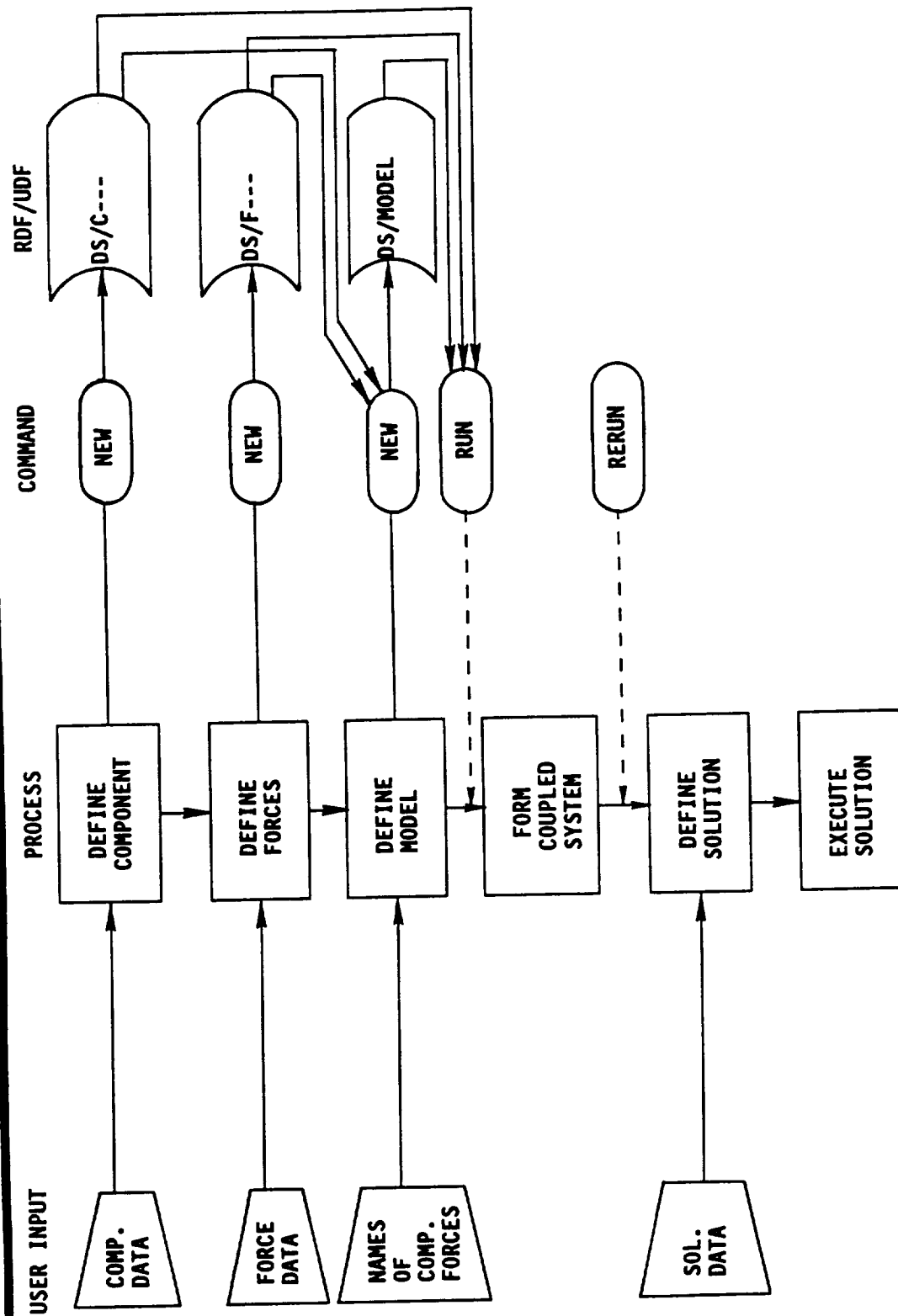


COMPONENT	NO.	DATA SET
CTR4	1	ABCD1
CTR4	3	ABCD1
CTR4	5	ABCD1
CTR4	2	ABCD2
CTR4	4	ABCD2
CTR4	6	ABCD2
CSF1	7	TOPR
CSF1	8	TOPL
CSF1	9	CONTR
CLC1	10	GROUND

DYSCO SYSTEM OVERVIEW



MODELING SCENARIO AND COMMAND RELATIONSHIP



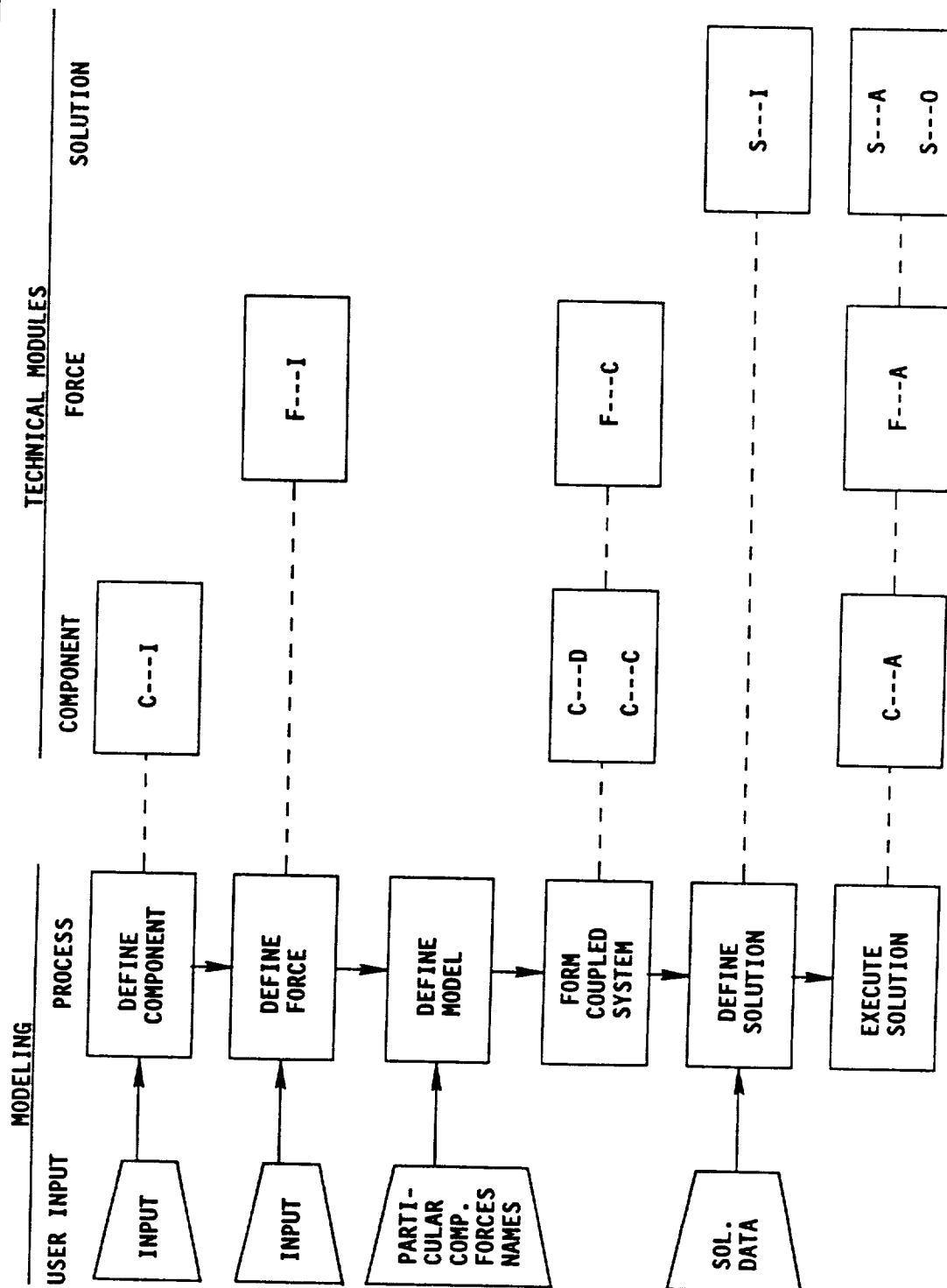
STANDARD TECHNICAL MODULES

<u>FUNCTION</u>	<u>COMPONENT</u>	<u>FORCE</u>	<u>SOLUTION</u>
INPUT	C---I	F---I	S---I
DEFINITION	C---D	N/A	N/A
COEFFICIENT	C---C	F---C	N/A
ACTIVE	C---A	F---A	S---A
OUTPUT	N/A	N/A	S---0
LOADS	C---L	N/A	N/A

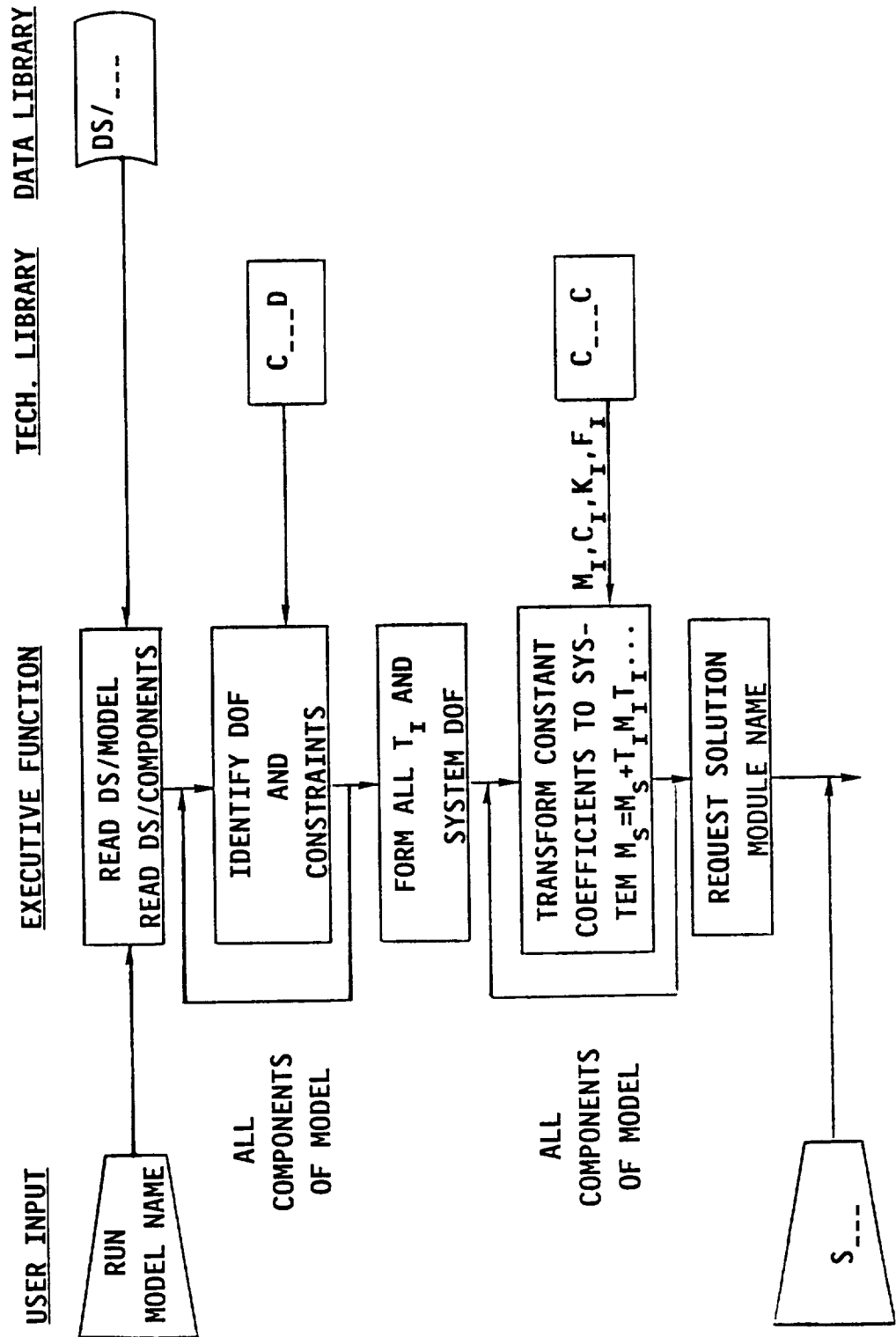
TECHNICAL MODULES

---I	INPUT DEFINITION
---D	DEFINE DEGREES OF FREEDOM
---C	COMPUTE CONSTANT COEFFICIENTS IN EQUATIONS
---A	COMPUTE NON-CONSTANT COEFFICIENTS, FUNCTION OF TIME AND STATE
---O	OUTPUT
---L	INTERNAL LOADS, FUNCTION OF STATE

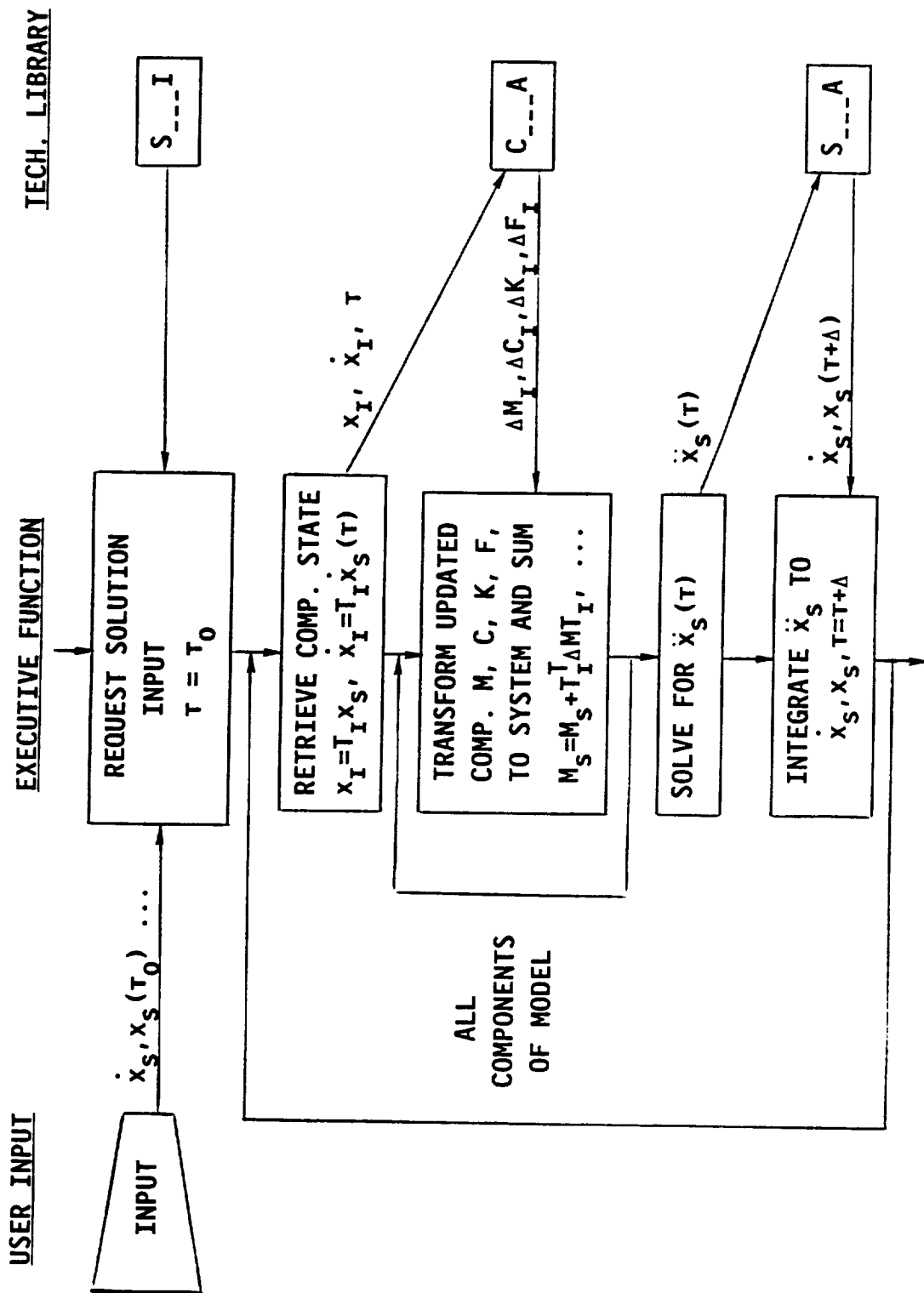
**RELATIONSHIP BETWEEN MODELING
SCENARIO AND TECHNICAL MODULES**



RUN COMMAND
(ASSEMBLY OF MODEL)



TIME HISTORY SCENARIO
(CONTINUATION OF RUN)



FEATURES OF EXECUTIVE

- o EXECUTIVE IS SPECIFICALLY BUILT TO MANAGE
STRUCTURAL DYNAMIC ANALYSIS
- o IT UNDERSTANDS AND MANAGES
 - INPUT: IDENTIFICATION, STORAGE, EDITING
 - MODEL BUILDING: RETRIEVAL OF DATA, CALLS
TO TECHNOLOGY LIBRARY
 - ASSEMBLY OF EQUATIONS: APPLIES MPC, SPC
 - SOLUTION OF EQUATIONS: CALLS TO TECHNOLOGY
LIBRARY, RETRIEVAL OF LOCAL STATES,
INTERFACE LOADS
- o EXECUTIVE INDEPENDENT OF ANY PARTICULAR AREA OF
TECHNOLOGY
 - UNIFORM ABSTRACT INTERFACES TO TECHNOLOGY
LIBRARY

- o NEW TECHNOLOGY EASILY ADDED
 - COMPONENT, FORCE, SOLUTION
 - UNIFORM INTERFACES TO EXECUTIVE
 - FORTRAN CODING
- o COMPONENTS ARE ANY SECOND ORDER ODE, SUCH AS,
 - SINGLE SPRING, DAMPER, OR MASS
 - ANY FINITE ELEMENT
 - COMPLETE NASTRAN MODEL
 - HELICOPTER ROTOR
 - MIMO CONTROL ALGORITHM
- o SOLUTIONS ACT ON MODEL EQUATIONS, E.G.
 - EIGENANALYSIS
 - FREQUENCY RESPONSE
 - TIME HISTORY
 - HELICOPTER TRIM (PERIODIC SHOOTING)
 - PERIODIC SYSTEM STABILITY
 - STATE FEEDBACK OPTIMIZATION

OTHER FEATURES

- 0 VALIDATED INPUT AND EDITING
 - USES KNOWLEDGE TABLE: TYPE, CHARACTERISTICS, EXISTENCE, RANGE
 - PROMPTED INPUT
 - INSTANTANEOUS VALIDATION
 - ASSURED COMPLETE AND CONSISTENT DATA
- 0 SIMPLE EDITING OF MODEL
 - CONFIGURATION CHANGES
 - PARAMETER VARIATION
 - DAMAGE ANALYSIS
- 0 INTELLIGENT COUPLING PROCEDURES
 - RECOGNITION OF DOF NAMES
 - MPC OPTIONALLY AUTOMATICALLY FORMED
 - GENERAL MPC SOLVED FOR DOF EQUATIONS

0 CSF1 - LINEAR FINITE ELEMENT

USER SUPPLIES: NAMES OF DOF
M, C, K, F

0 CFM3 - 3D MODAL STRUCTURE

RIGID BODY, ELASTIC MODES (ALL OPTIONAL)
DOF NAMES AUTOMATICALLY GENERATED
AUTOMATIC COUPLING AT SPECIFIED NODES

0 CSB2 - GENERAL BAR ELEMENT* (NOT AVAILABLE IN GOVT VERSION)

MAY BE USED AS A BEAM OR ROD ELEMENT
SHEAR FACTORS, CONSISTENT MASS, RAYLEIGH DAMPING
UP TO 12 DOF

DYSCO
BASIC TECHNOLOGY MODULES (CONT'D)

- 0 CES1 - ELASTIC STOP
NONLINEAR SPRING, DAMPING, WITH GAP
- 0 CGF2 - GENERAL FORCE
 - POLYNOMIAL, FOURIER SERIES, OR TABULAR
 - PERIODIC
- 0 CLC0 - SINGLE POINT CONSTRAINTS
- 0 CLC1 - MULTIPOINT CONSTRAINTS
- 0 CLC2 - ADVANCED MULTIPOINT CONSTRAINT

0 SEA4 - EIGENANALYSIS, REAL

0 SEA5 - COMPLEX EIGENANALYSIS

0 STH4 - TIME HISTORY
- CONDITION CODES

0 SFD1 - FREQUENCY DOMAIN MOBILITY
- RESPONSE PER UNIT FORCE

0 STC0 - OPTIMIZER FOR LINEAR STATE FEEDBACK* (NOT
AVAILABLE IN GOVT VERSION)
- SOLVES MATRIX RICCATI EQUATION
- INTEGRATES SYSTEM STATE EQUATIONS

0 SII3 - INTERFACE AND INTERNAL LOADS
- RESIDUAL FORCES AT INTERFACES
- FORCES, STRAIN ENERGY, BENDING MOMENTS

0	CRR2, CRR3 - HELICOPTER ROTOR
0	CCE0, CCE1 - ROTOR CONTROL SYSTEM
0	CRD3 - ROTOR DAMAGE
0	CFM2 - HELICOPTER FUSELAGE
0	CLG2 - NONLINEAR LANDING GEAR
0	CLS2 - LIFTING SURFACE
0	FRA0, FRA2, FRA3 - ROTOR AERODYNAMICS
0	FFA0, FFC2 - FUSELAGE AERODYNAMICS
0	STH3 - TIME HISTORY, HELICOPTER CONTROLS
0	STR3 - HELICOPTER TRIM
0	SSF3 - FLOQUET STABILITY

DYSCO AND FE CODES

- 0 DYSCO DOES NOT COMPETE WITH FE CODES
- 0 DYSCO COMPLEMENTS FE CODES
- 0 FE ANALYSIS FOR DETAILED STRUCTURAL ANALYSIS
- 0 DYSCO CAN START WITH FE MODEL AND:
 - MODIFY CONFIGURATION
 - SIMULATE DAMAGE
 - ADD CONTROL ALGORITHMS
 - ADD SPECIAL COMPONENTS
 - PERFORM SOLUTIONS ON ALL MODIFICATIONS
 - STUDY EFFECTS OF CHANGE
 - ANALYZE CONFIGURATIONS NOT POSSIBLE (OR CONVENIENT) WITH FE CODES
- 0 DYSCO CAN ALSO MODEL STRUCTURES ON ITS OWN

WHAT DYSCO CAN DO FOR YOU

- o SIMPLE PROBLEMS ARE EASY AND INEXPENSIVE TO SOLVE
- o PROBLEMS NOT CONVENIENTLY MODELED ELSEWHERE CAN BE SOLVED
- o PHENOMENA CAN BE BETTER UNDERSTOOD:
 - START WITH SIMPLE REPRESENTATION
 - GRADUALLY INCREASE COMPLEXITY
 - VARY PARAMETERS
 - VARY CONFIGURATION
- o NOVEL CONCEPTS CAN BE EASILY MODELED AND EVALUATED
- o NEW ALGORITHMS CAN BE TESTED AND EVALUATED

LIST OF ILLUSTRATIVE PROBLEMS

- 0 PACOSS TOWER DYNAMIC ANALYSIS
- 0 TRUSS STRUCTURE WITH ACTIVE ELEMENTS - VIBRATION CONTROL
- 0 PIEZOELECTRIC SENSORS/ACTUATORS ON BEAM - VARY CONTROL LAWS, ADD ELASTIC STOP, STABILITY, TIME, FREQUENCY DOMAIN
- 0 POINTING-TRACKING SYSTEM - MOTOR DRIVEN MIRRORS - MOVING, ACCELERATING TARGET, VARY CONTROL GAINS
- 0 ROTORCRAFT TRIM - DAMAGED BLADE - INTERNAL LOADS
- 0 RAIL GUN PNEUMATIC ACCELERATOR - GAS PRESSURE - BOLT MOTION
- 0 ALGORITHM EVALUATION - REDUCED MODELS, SYSTEM IDENTIFICATION, SIMULATE EFFECTS OF MEASUREMENT ERRORS

DYSCO MODELING

o DYSCO COUPLES THE EQUATIONS OF INDIVIDUAL COMPONENTS TO FORM THE EQUATIONS OF A MODEL

o EACH COMPONENT AND MODEL ARE OF THE FORM

$$M\ddot{X} + C\dot{X} + KX = F$$

$$M, C, K, F = F(T, \dot{X}, X)$$

o M, C, K, F MAY BE ARBITRARY FUNCTIONS OF TIME OR STATE

o X MAY REPRESENT PHYSICAL, MODAL, OR ANY GENERALIZED DOF

o EACH COMPONENT IS REPRESENTED BY FORTRAN SUBROUTINES IN THE TECHNOLOGY LIBRARY

- 0 DYSCO USES AN "INTELLIGENT" PROCEDURE FOR
COUPLING DEGREES OF FREEDOM
- 0 DEGREES OF FREEDOM OF COMPONENTS MAY BE:
 - PHYSICAL COORDINATES
 - MODAL DISPLACEMENTS
 - ANY GENERALIZED COORDINATES
- 0 COUPLING INCLUDES
 - PHYSICAL TO PHYSICAL
 - PHYSICAL TO MODAL
 - MODAL TO MODAL
 - SINGLE POINT CONSTRAINTS
 - MULTIPLE POINT CONSTRAINTS
 - ANY LINEAR RELATIONSHIPS
- 0 EFFECTS SIMULATED
 - RIGID PHYSICAL LINKAGES
 - OPTICAL BEAM COORDINATES
 - CONTROL ALGORITHMS

COUPLING

X , X_I ARE VECTORS OF THE DOFS OF THE SYSTEM (MODEL) AND
THE COMPONENTS

T_I IS A TRANSFORMATION MATRIX

$$X_I = T_I X$$

THE EQUATION OF THE MODEL IS

$$MX + CX + KX = F$$

WHERE

$$M = \sum T_I^T M_I T$$

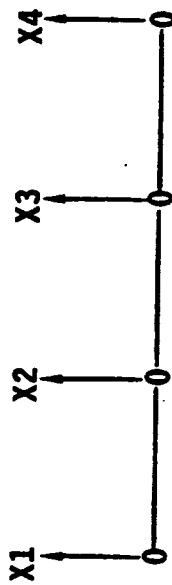
$$C = \sum T_I^T C_I T$$

$$K = \sum T_I^T K_I T$$

$$F = \sum T_I^T F_I$$

EACH T_I IS AUTOMATICALLY FORMED IN DYSCO

- 0 DYSCO USES A UNIQUE PROCEDURE WHERE VARIABLE NAMES (A4, I4) ARE RECOGNIZED AND PROCESSED
- 0 NAMES ARE AUTOMATICALLY FORMED OR USER SUPPLIED
- 0 LIKE NAMES IN COMPONENTS IMPLY CONNECTION
- 0 SIMPLE EXAMPLE:



TO CONSTRAIN X3 TO GROUND BY A SPRING, K, USER SIMPLY ADDS COMPONENT TO MODEL WITH FOLLOWING INFORMATION

NO OF DOF = 1
NAME = X3
M = C = F = NULL
K = K

SIMPLE CONTROL SYSTEM EXAMPLE



SENSOR LOCATIONS X1, X4, X6
ACTUATOR LOCATIONS X3, X4

$$\dot{F}_{X3} = A \cdot X1 + B \cdot X4 + C \cdot X6 + D \cdot \dot{X4}$$

$$\dot{F}_{X4} = E \cdot \dot{X1} + F \cdot X6 + G \cdot \dot{X6}$$

THIS MAY BE REPRESENTED BY COMPONENT WITH

$$DOF = [X1, X3, X4, X6]$$

$$M = 0$$

$$C = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & D & 0 \\ E & 0 & 0 & G \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$K = \begin{bmatrix} 0 & 0 & 0 & 0 \\ A & 0 & B & C \\ 0 & 0 & 0 & F \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

SENSOR AND ACTUATOR LOCATIONS MAY BE CHANGED BY EDITING
DOF NAMES. GAINS MAY BE CHANGED BY EDITING MATRICES.

- o COUPLING MAY ALSO USE OPTIONAL LINEAR RELATIONS
- o SINGLE POINT, MULTIPOINT, CONNECTIVITY CONSTRAINTS
 - $X1 = 1.0 * X2$
 - $X10 = 0$
- $A * X10 + B * Y100 + C * Z20 = 0$
- o REPRESENTATION OF MECHANICAL LINKAGES
- o CONVERSION TO CONVENIENT PARAMETERS
 - OPTICAL BEAM ANGLE AS FUNCTION OF MIRROR DOF
 - TIP DISPLACEMENT OF BEAM AS FUNCTION OF MODAL DOF

DYSCO IS A DOMAIN EXECUTIVE CONTROL SYSTEM

THE DOMAIN IS "COUPLED DYNAMIC EQUATIONS"

IT EXECUTES TECHNICAL MODULES IN "PARALLEL"
(RATHER THAN IN SEQUENCE)

SIMPLE COMMANDS PERFORM NUMEROUS MODULE
EXECUTIONS (E.G., RUN)

INVALID COMMAND SEQUENCES ARE NOT ACCEPTED
INVALID DATA USAGE IS NOT POSSIBLE

ALL DATA PLACED ON FILES OR EDITED IS ASSURED TO BE
VALID (E.G., CONSISTENCY AND FORMAT)

TERMINOLOGY

- 0 COMPONENT - ALGORITHM FOR COMPUTING M, C, K, F FOUND IN TECHNOLOGY LIBRARY

NAME: C---

- 0 DATA SET - SPECIFIC SET OF DATA TO BE USED WITH A COMPONENT FOUND IN DATA LIBRARY. INPUT BY USER. USER SUPPLIES DATA SET "NAME"
- 0 MODEL - COLLECTION OF COMPONENTS AND ASSOCIATED DATA SETS

SAMPLE MODEL

<u>COMPONENT</u>	<u>DATA SET</u>
CSF1	STRUT1
CSF1	STRUT2
CFM2	FUSELAGE
CSF1	CONTROL 3
CES1	K100

MODEL PATIE12

***** MODEL PATIE12 *****

CATSTAR: SAME AS PATIE11 BUT CLC1 REWRITTEN FOR PHIP1 IMPLICIT

INDEX	COMP	NO.	DATA SET	FORCE	DATA SET
1	CSF1		PRIMARY	NONE	
2	CSF1		BASE P-S	NONE	
3	CSF1		SECONDARY	NONE	
4	CSF1		BASE S-M	NONE	
5	CSF1		MUTOK	NONE	
6	CSF1		TRUSS-PR	NONE	
7	CSF1		TRUSS-DI	NONE	
8	CSF1		TRUSS-MD	NONE	
9	CFM2	1	SHUTTLE	NONE	
10	CSF1		CONTROL1	NONE	
11	CSF1		TARGET	NONE	
12	CSF1		NUMAL	NONE	
13	CLC1		OPTICS3	NONE	

***** GLOBAL VARIABLES *****

***** NO INPUT REQUIRED *****

CONTROL1/CSF1

```

*****
CONTROL LAW 1 FOR GIMBALLED MIRROR
*****
*****
INPUT FOR COMPONENT CSF1. FINITE ELEMENT
*****
1 NCDF      - NUMBER OF DOF      =      3
2 CDFLI      - (DOF) DOF NAME
      PHIP1000  DSTR1000  MTH 1000
3 CM      - (REAL) MASS MATRIX VALUES
      NULL MATRIX
4 CC      - (REAL) DAMPING MATRIX VALUES
      GENERAL MATRIX
      ROW      1      NULL ROW
      ROW      2
      3.70000E+02  0.00000E+00  0.00000E+00
      ROW      3
      -3.70000E+02  0.00000E+00  0.00000E+00
5 CK      - (REAL) STIFFNESS MTRX VALUES
      GENERAL MATRIX
      ROW      1      NULL ROW
      ROW      2
      1.23300E+06  0.00000E+00  0.00000E+00
      ROW      3
      -1.23300E+06  0.00000E+00  0.00000E+00
6 CF      - (REAL) FORCE VECTOR VALUES
      0.00000E+00  0.00000E+00  0.00000E+00
*****
*****

```

HELIUM1/CAG1
HELIUM ACCUMULATOR FOR ET1 MODEL

```

*****
HELIUM1 /CAG1 *****
HELIUM ACCUMULATOR FOR ET1 MODEL

*****
INPUT FOR COMPONENT CAG1. ADIABATIC GAS *****

1 NCDF      - NUMBER OF DOF      =      3
2 CDFLI      - (DOF) DOF NAME
  PROJ1000 BOLT1000 MAGZ1000
3 GVECT      - (REAL) INITIAL GAS VECTOR
  4.55000E+03  4.00000E+00  1.66700E+00  2.07703E+00
  8.40000E+04
4 AREA      - (REAL) MATRIX FOR AREA CALC
  GENERAL MATRIX

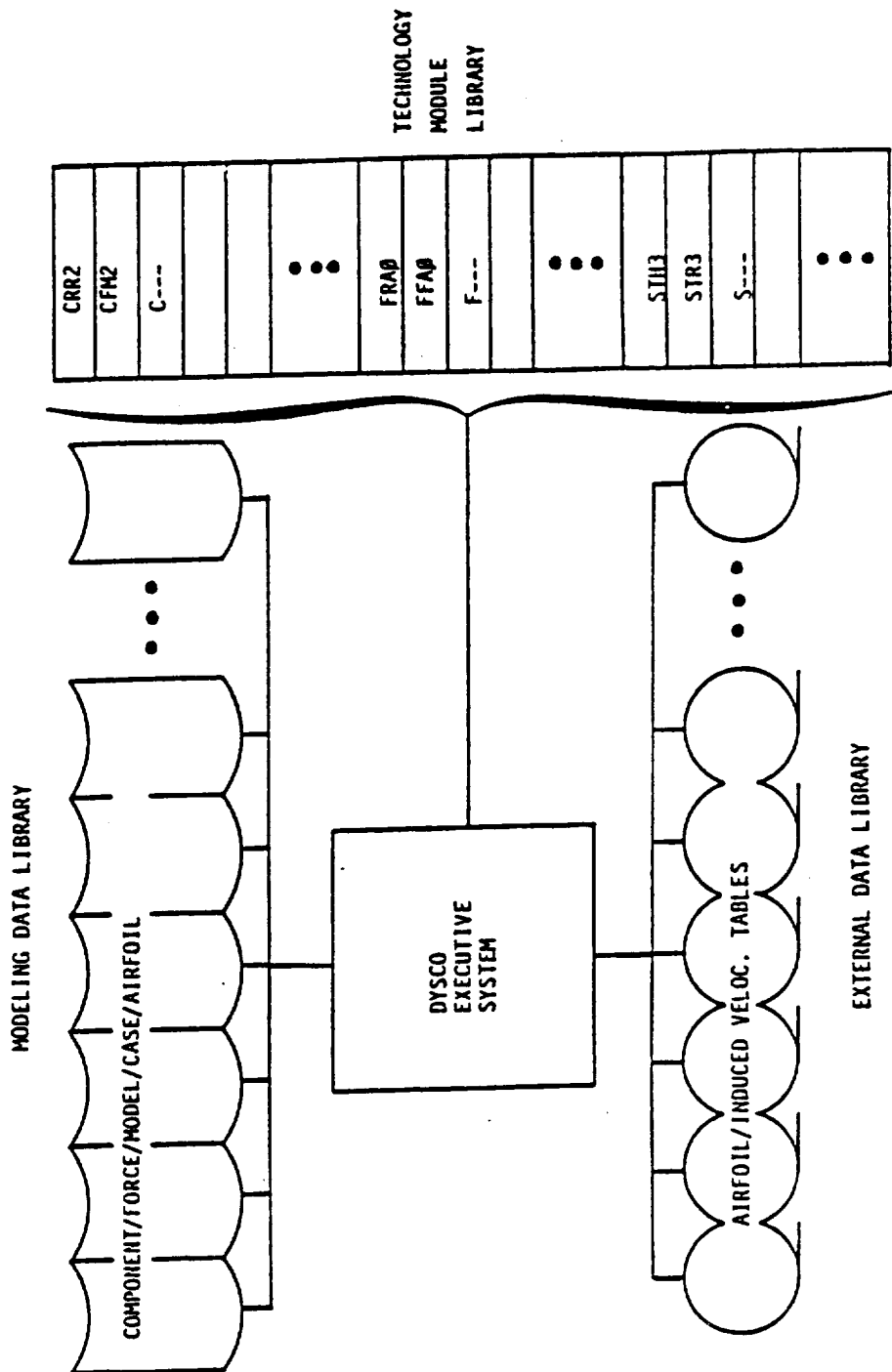
ROW 1
2.00000E+00  2.00000E+00  3.00000E+00

ROW 2
1.00000E+00  1.00000E+00  6.66670E-01
5 GOVDOF      - (DOF) AREA EXIST CRITERIA
  PROJ1000 BOLT1000 BOLT1000
6 AECV      - (REAL) GOVDOF CRITICAL VALU
  -1.00000E+04 -1.00000E+04  1.00000E+00
7 PECDOF      - PRESSURE EX CRITERIA= PROJ1000
8 PECVAL      - CRITICAL VALUE      = 7.75000E+00
*****

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- 0 TECHNOLOGY LIBRARY CONTAINS
 - COMPONENT REPRESENTATIONS (C ...)
 - FORCE ALGORITHMS (F ...)
 - SOLUTION ALGORITHMS (S ...)
- 0 DATA LIBRARIES CONTAIN
 - DATA ASSOCIATED WITH PARTICULAR C ..., F ...
 - AND IDENTIFIED BY DATA SET NAME
 - SUPPLIED BY USER

DYSCO LIBRARIES



ANY TECHNOLOGY MODULE MAY BE ADDED TO LIBRARY IF:
COMPONENT, FORCE

M, C, K, F MAY BE COMPUTED AS FUNCTIONS
OF LOCAL STATE VECTOR AND TIME BY A
FORTRAN PROGRAM

SOLUTION

ALGORITHM MAY BE WRITTEN IN FORTRAN, GIVEN
SYSTEM M, C, K, F, AS ABOVE

TYPICAL COMMANDS

COMMAND

NEW	ALLOWS USER TO MODIFY MODEL ALLOWS USER TO CREATE NEW COMPONENT/FORCE INPUT DATA
RERUN	NEW SOLUTION FOR MODEL JUST RUN
RUN	FORMS EQUATIONS OF MODEL AND EXECUTES A SOLUTION
EDIT	ALLOWS USER TO TO MODIFY MODEL AND PERFORM VALIDATED EDIT OF INPUT DATA

ABSTRACT BASIS OF DYSCO

DYSCO ACHIEVES ITS MULTIPURPOSE CAPABILITY BY A COMPLETE SEPARATION OF ABSTRACT AND SPECIFIC DATA.

SINCE DYSCO DOES NOT TREAT SPECIFIC PHYSICAL COMPONENTS, FORCES, OR SOLUTIONS, IT CAN SOLVE PROBLEMS INVOLVING ANY COMPONENTS, FORCES, OR SOLUTIONS.

THE USER PERCEIVES A "MODEL" MADE UP OF COMPONENTS

HE THEN:

SELECTS APPROPRIATE REPRESENTATIONS FOR EACH
COMPONENT FROM THE LIBRARY

SELECTS APPROPRIATE FORCE ALGORITHMS FOR EACH
COMPONENT

SELECTS APPROPRIATE SOLUTION METHODS.

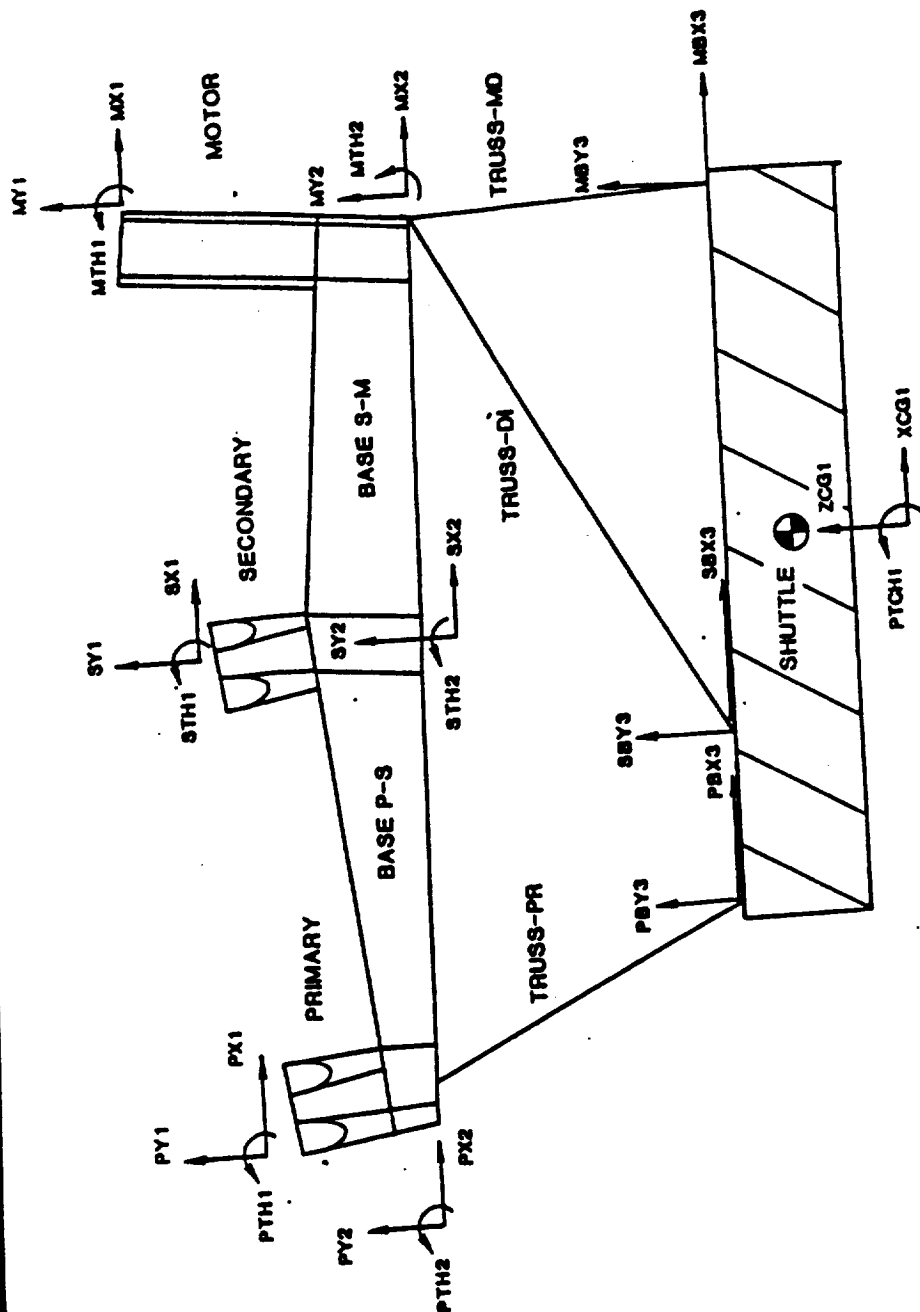
NOTE THAT THE ORIGINAL MODEL FORMULATION REQUIRES AN APPROPRIATE LEVEL
OF ENGINEERING JUDGEMENT.

FOR EACH COMPONENT AND FORCE, THE DATA MUST BE IDENTIFIED AS RESIDING
ON A USER FILE OR THE DATA MUST BE PLACED ON A FILE USING DYSCO.

THE MODEL AND VARIATIONS MAY THEN BE FORMED INTERACTIVELY AND SPECI-
FIED SOLUTIONS MAY BE CARRIED OUT.

ILLUSTRATIVE APPLICATIONS

DYSCO 2D STRUCTURAL MODEL



MODEL 1 18 DOF (GROUNDED)
2-5 VARIOUS BASE SHAKES
6 21 DOF (3 BASE DOF)

CONTROL GAINS

I. MAX TORQUE FOR MOTOR AT MAX RATE .05 R/S - 370 IN #

II. DESIGN TORQUE $T = 185$ IN #

III. INITIAL TRIAL GAINS

1. DISPLACEMENT GAIN

IF ϕ IS AT A MAX ALLOWABLE ERROR OF $15 \mu R$, LET MOTOR BE
DRIVEN AT MAX SPEED

$$T = 185 \text{ IN \# AT } 15 \mu R$$

$$K_2 = 1.233 \times 10^7 \text{ IN \# / R OF } \phi$$
$$= 0 \text{ IN \# AT } 0$$

2. VELOCITY GAIN

IF $\dot{\phi}$ IS AT MAX RECESSION OR APPROACH OF .05 R/S, LET
MOTOR BE DRIVEN AT MAX SPEED

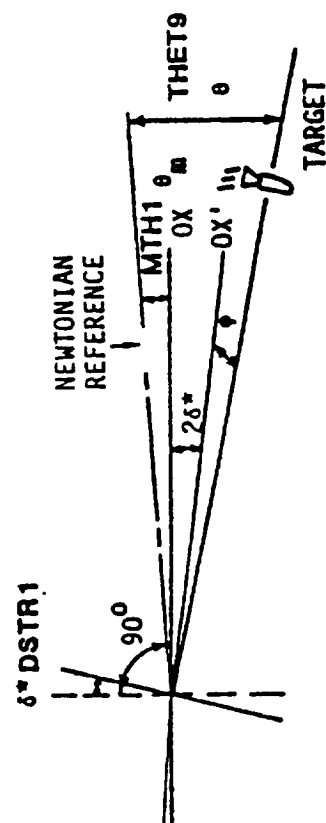
$$T = 185 \text{ IN \# AT } .05 \text{ R/S}$$

$$K_1 = 3.7 \times 10^3 \text{ IN \# SEC/R OF } \phi$$
$$= 0 \text{ IN \# AT } 0$$

TYPICAL STRUCTURAL VARIABLES MONITORED

I. MIRROR AND MOTOR

1. $\text{THET9} = \theta$ = TARGET L.O.S. FROM INERTIAL REFERENCE
2. $\text{DSTR1} = \delta^* = \text{ACTUAL DRIVE ANGLE OF MIRROR}$
3. $\text{MTH1} = \theta_M = \text{STRUCTURAL VIBRATION OF THE MOTOR MOUNT}$
4. $2\delta^* + \theta_M = \text{OX}'$ (BENT OPTICAL AXIS) FROM INERTIAL REFERENCE
5. $\phi = \theta - \theta_M - 2\delta^* = \text{OPTICAL MISPOINT}$



CASE 1 TIME HISTORY
(PAGE 1 OF 3)

CASE 1 TIME HISTORY

STATIONARY TARGET AT ZERO

INITIAL LINES-OF-SIGHT STATIONARY

Solid - Optical Mispoint of Flat Mirror

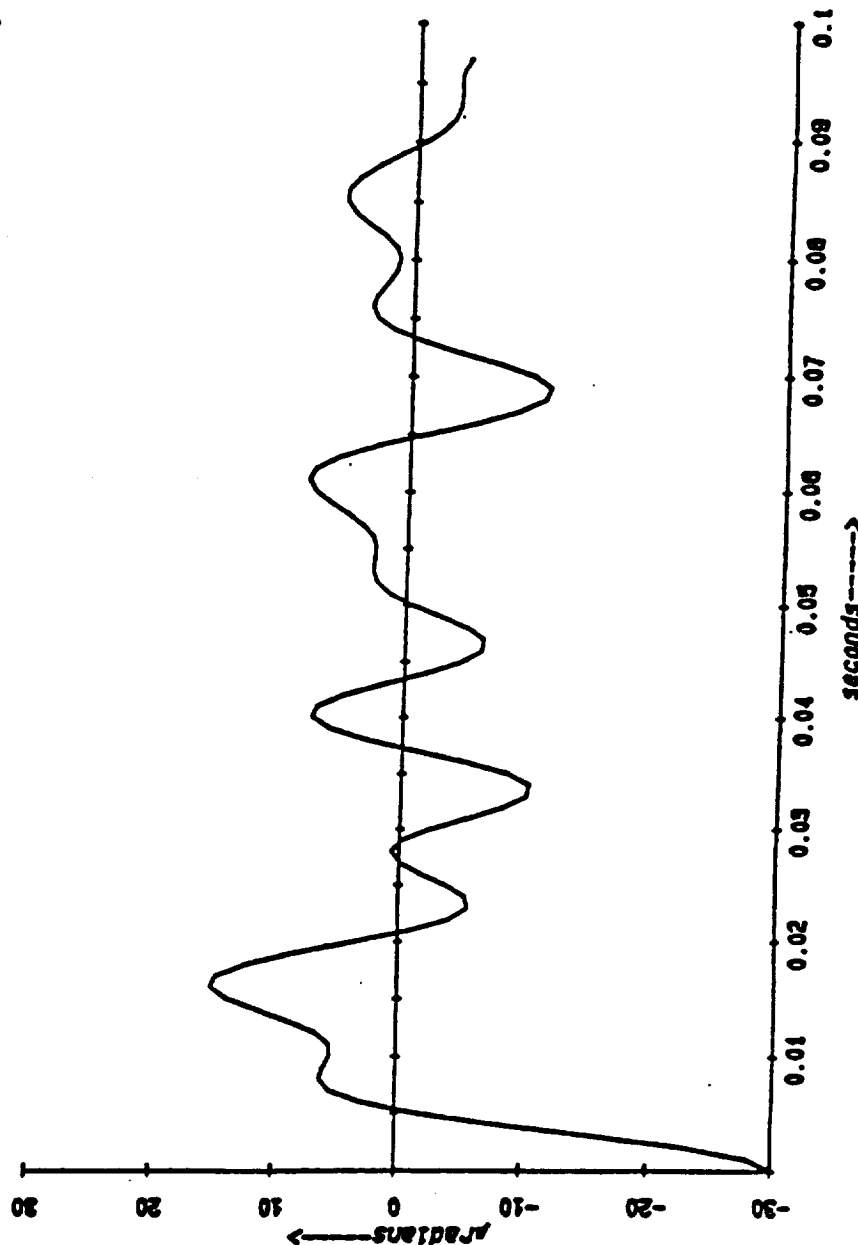
----- INITIAL MISPOINT DSIR = 15 μ rad

CONTROLS:

Displ. Gain = Max Avail.

Vel. Gain = Max Avail.

KAMAN



CASE TIME HISTORY
(PAGE 2 OF 3)

KAMAN

CASE 8 TIME HISTORY

ACCELERATING TARGET ----- INITIAL MISPOINT DSIR = 15 μ rad

INITIAL LINES-OF-SIGHT APPROACHING

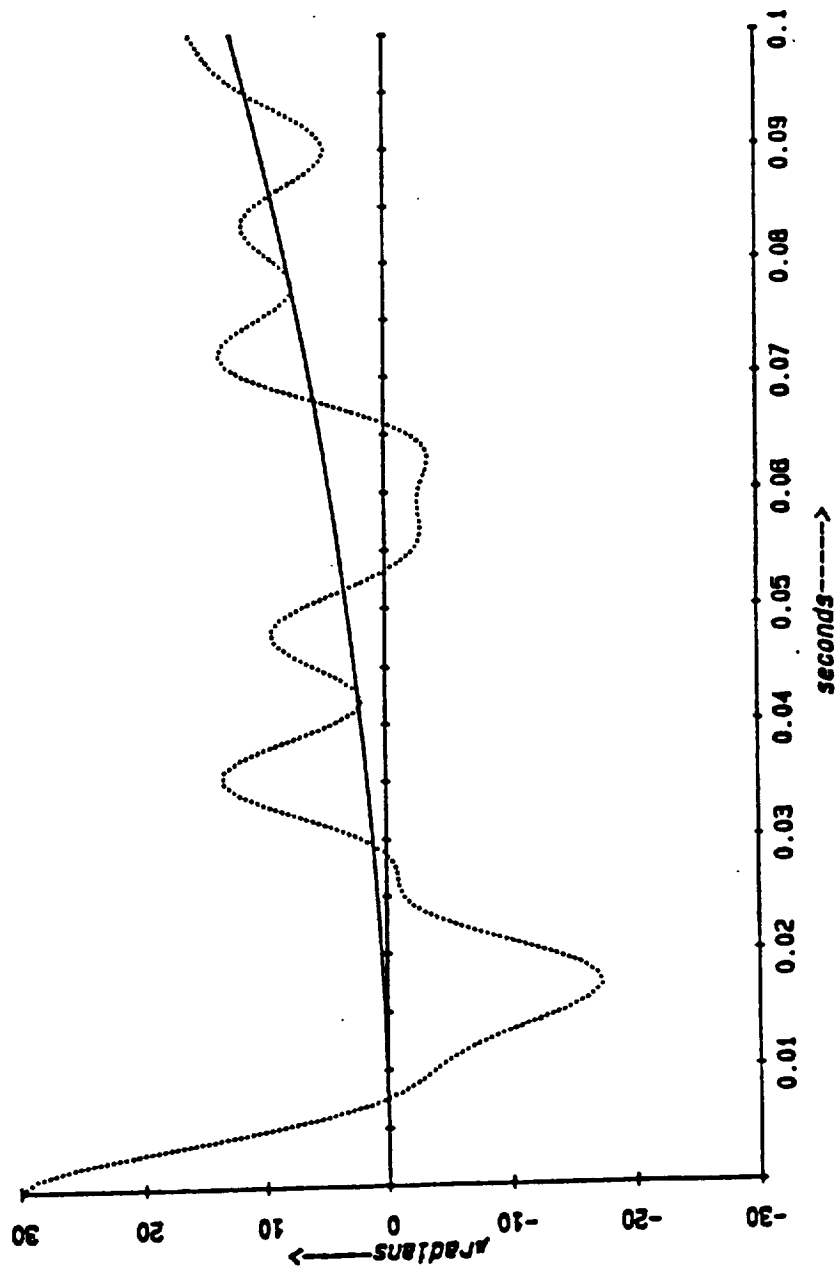
Solid - Target

Dotted - Pointing Axis L.O.S.

CONTROLS:

Displ. Gain = .65Max

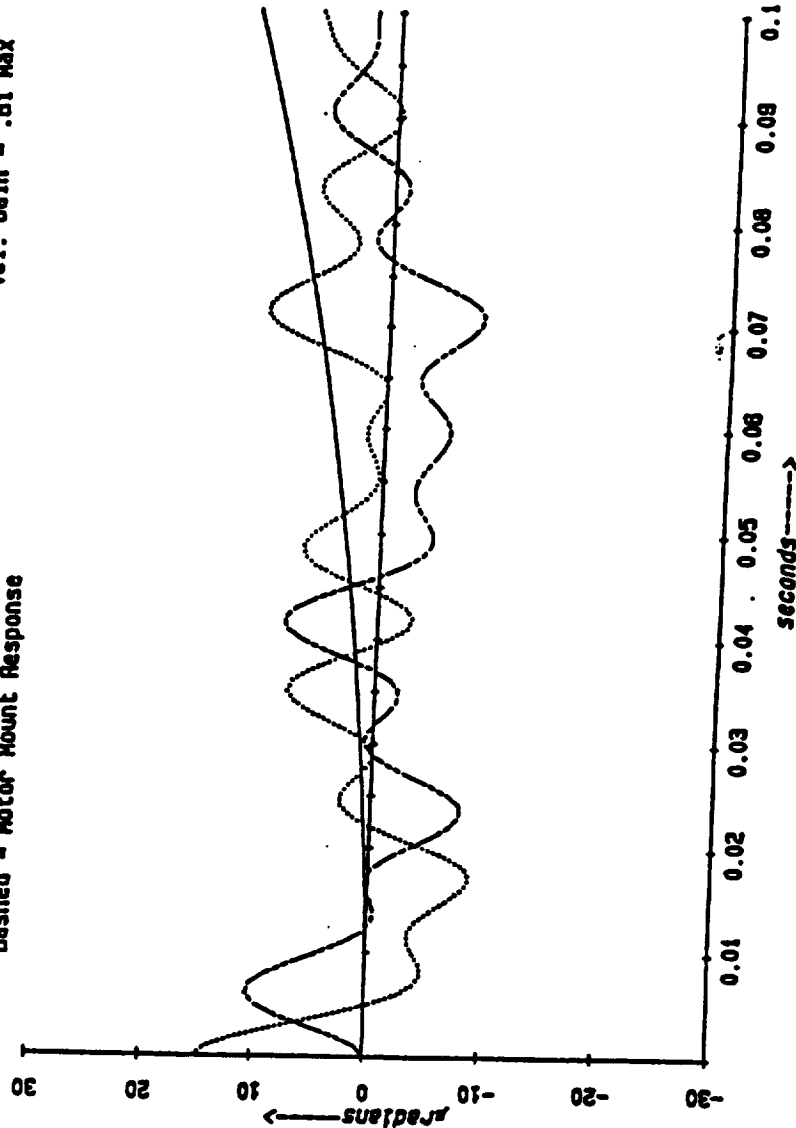
Vel. Gain = .81 Max



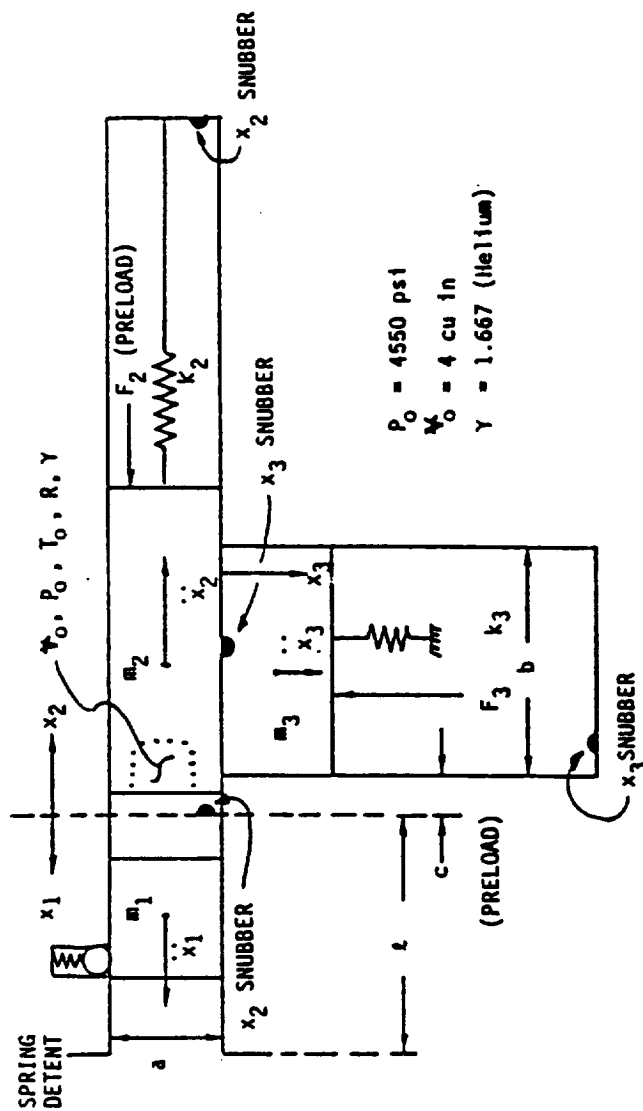
CASE TIME HISTORY
(PAGE 3 OF 3)

CASE B TIME HISTORY
ACCELERATING TARGET ----- INITIAL MISPOINT DSTR = 15 μ rad
INITIAL LINES-OF-SIGHT APPROACHING
Solid = Target
Dotted = Driven Mirror Angle
Dashed = Motor Mount Response

KAMAN
CONTROLS:
Displ. Gain = .85 Max
Vel. Gain = .81 Max



RAIL GUN PNEUMATIC PRE-ACCELERATOR



$P_0 = 4550$ psi
 $V_0 = 4$ cu in
 $\gamma = 1.667$ (Helium)

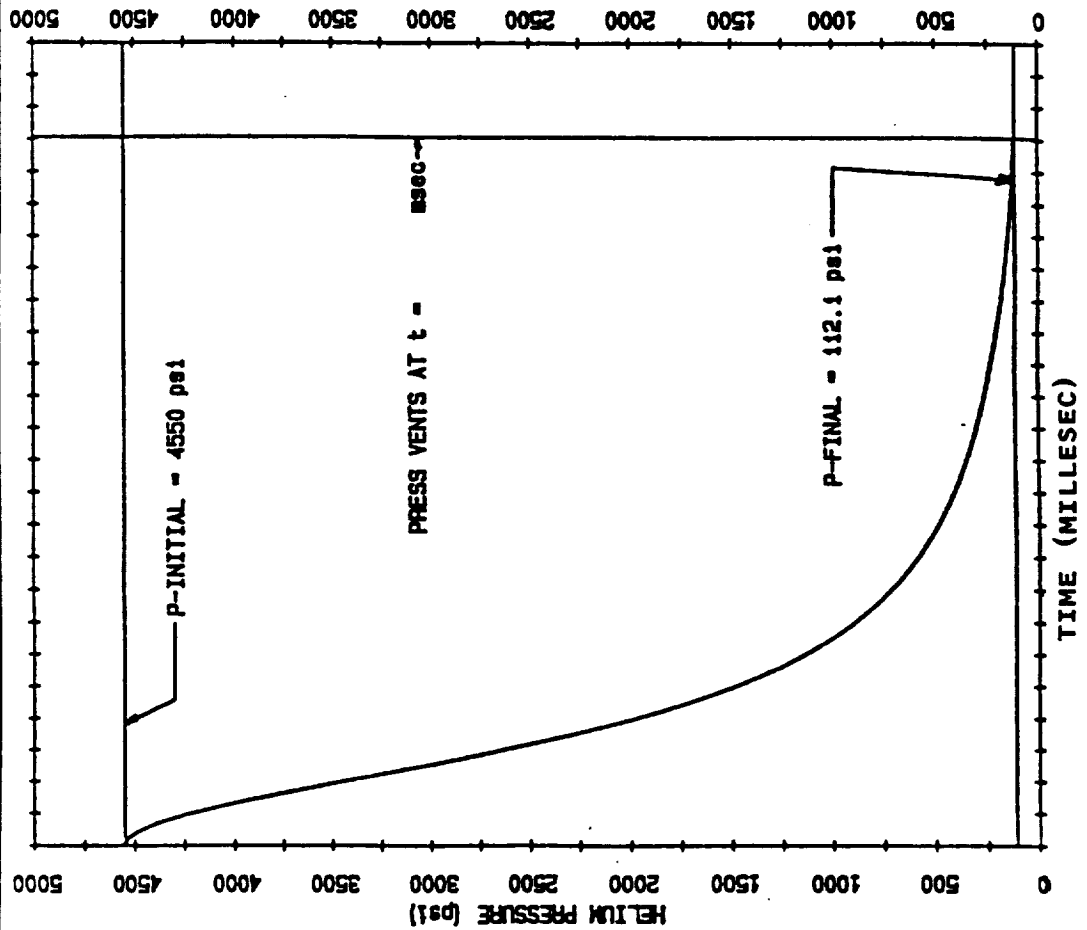
$m_1 =$ PROJECTILE $m_2 =$ BREECH BOLT $m_3 =$ MAGAZINE STACK

EQUATION OF MOTION -

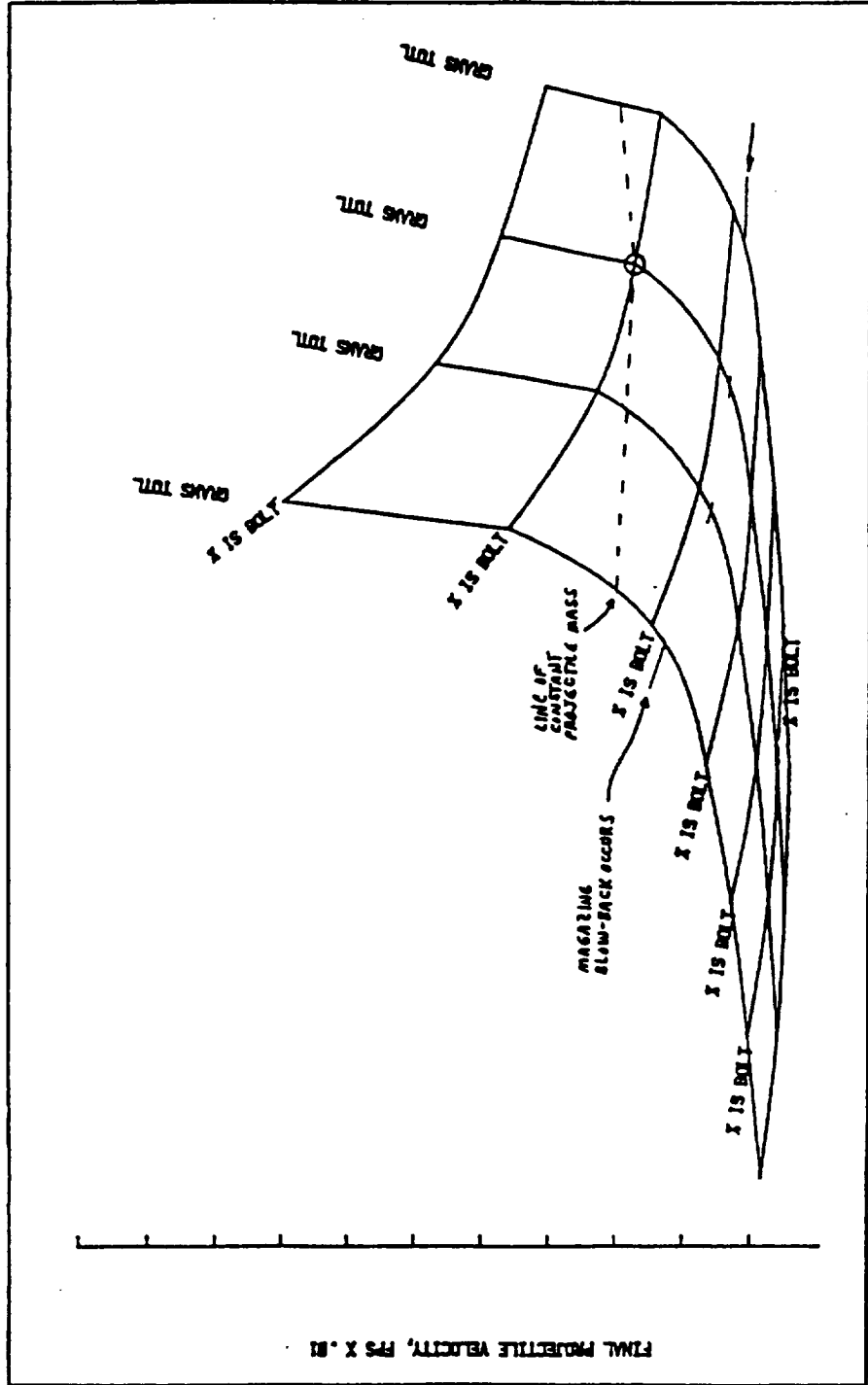
$$\begin{bmatrix} m_1 & 0 & 0 \\ 0 & m_2 & 0 \\ 0 & 0 & m_3 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \\ \ddot{x}_3 \end{Bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{Bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{Bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ k_2 & 0 & 0 \\ 0 & k_2 & k_3 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \\ x_3 \end{Bmatrix} = \begin{Bmatrix} A_1 P(t) \\ A_2 P(t) - F_2 \\ A_3 P(t) - F_3 \end{Bmatrix}$$

$A_3 = 0$ UNLESS
 $x_2 > c$ BEFORE
PRESSURE VENTS

**ET PRE-ACCELERATOR
PRESSURE CASCADE**

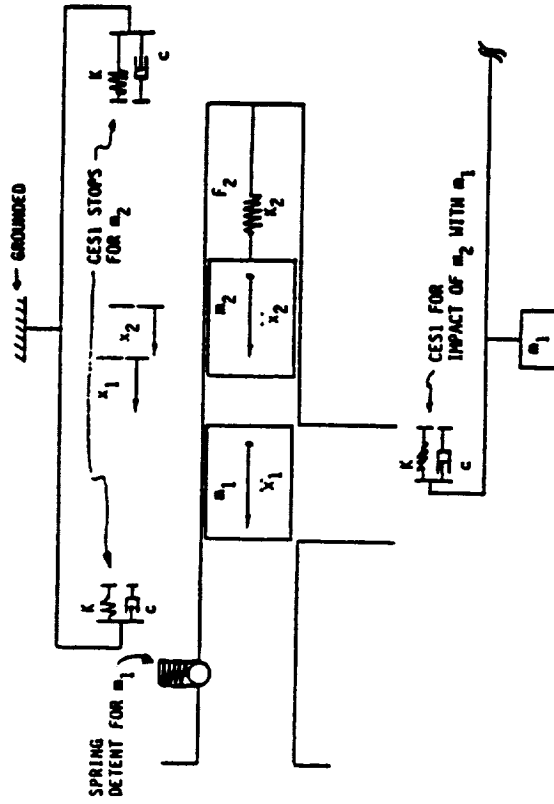


TRADES STUDIES FOR PRE-ACCELERATOR



ET PREACCELERATOR, BEHAVIOR VS. TOTAL
MASS AND PERCENT ALLOTTED TO BOLT

**MODEL FOR HARMONIC BOLT RETURN AND IMPACT WITH
FRESHLY LOADED PROJECTILE**

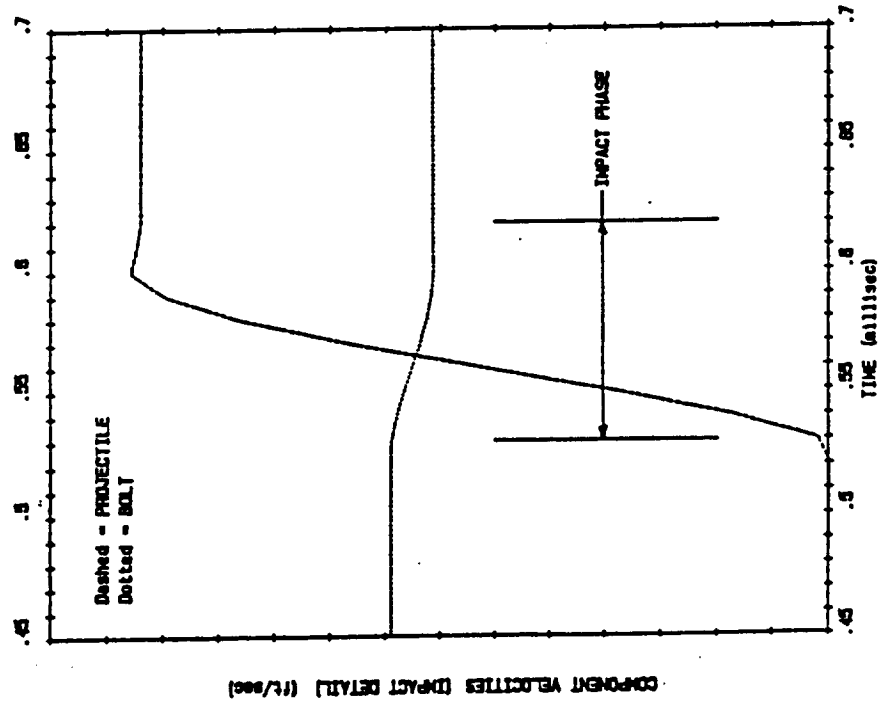


VARIOUS COEFFICIENTS OF RESTITUTION CAN BE
MODELLED BY JUDICIOUS CHOICE OF K AND C

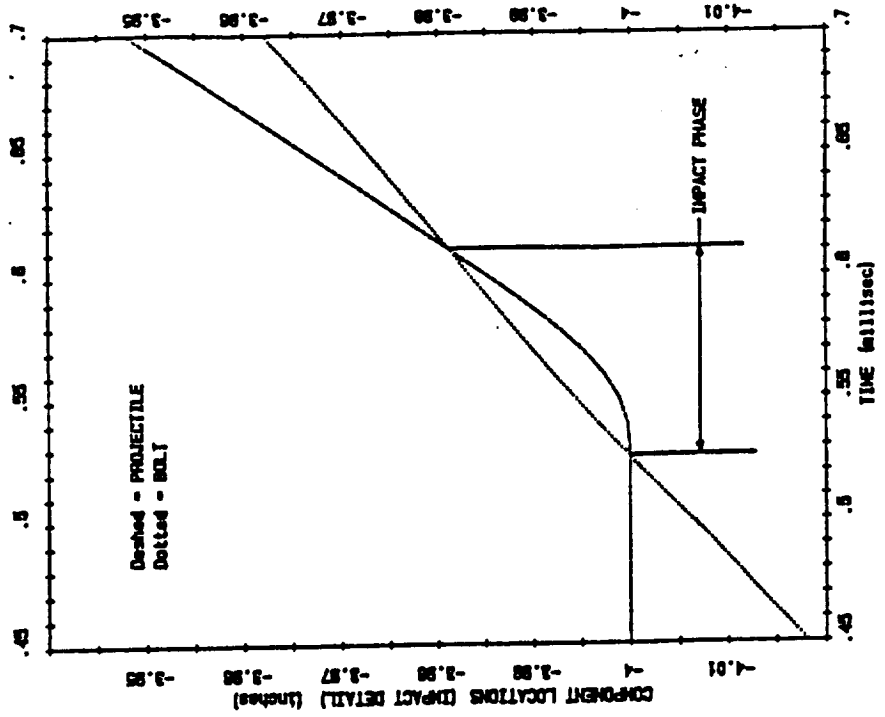
***** MODEL IMPACT 2 *****
IMPACT MODEL PLUS BARREL FIT/MAGAZINE FRICTION AND BALL SPRING DETENT

INDEX	COMP	NO.	DATA SET	FORCE	DATA SET
1	CSF1		BRIDYN	NONE	
2	CES1		BOLT2.0	NONE	
3	CSD1		BALL2	NONE	
4	CDF1		IMPMU	NONE	

IMPACT DETAIL
DISPLACEMENT AND VELOCITY



ET PRE-ACCELERATOR
TIME DOMAIN VELOCITIES



ET PRE-ACCELERATOR
TIME DOMAIN DISPLACEMENTS

